

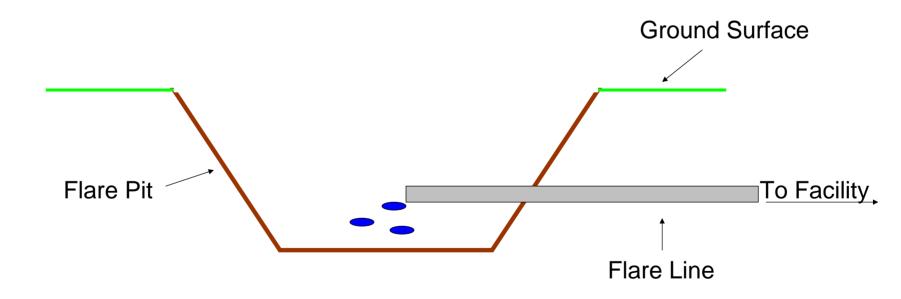
Interaction of Collected Water and Soil Within Remediation Excavations at Several Locations in Central Alberta







Earthen pits, also known as flare pits are a legacy of historical operations at oil and gas sites in Alberta







In the mid-1990's the ERCB (formerly the EUB) amended regulations and prohibited the use of earthen pits

Rough estimates put the number at well over 150,000 pits in Alberta





resources & energy







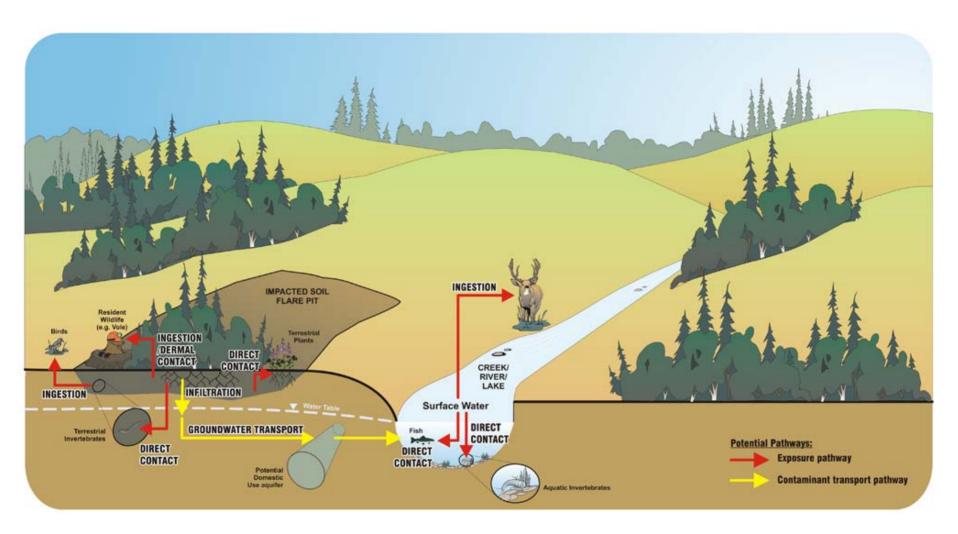












WorleyParsons

Flare Pit Excavations

resources & energy











Worley Parsons resources & energy

Contaminants













Worley Parsons resources & energy

Remediation





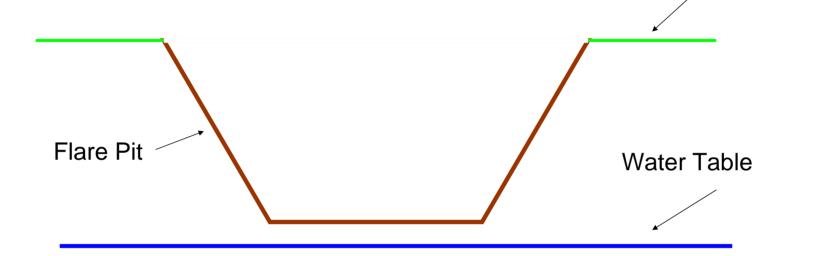


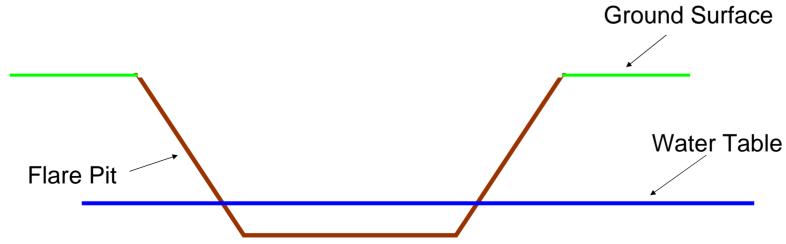




Water Table

Ground Surface









Water also collects as a result of rain and snow fall event



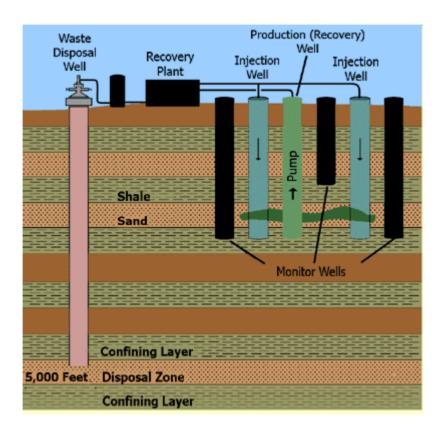












Leachate = Deep Well Injection



Infiltration

The Water Cycle



Water storage in ice and snow

Water storage in the atmosphere

Condensation

Precipitation

Evapotranspiration

Evaporation

Snowmelt runoff to streams

Surface runoff

Streamflow

Evaporation

Spring

Ground-water discharge

Sublimation

Water storage in oceans

U.S. Department of the Interior U.S. Geological Survey

Ground-water storage

Illustration by John M. Evans, USC http://ga.water.usgs.gov/edu/watercycle.htm





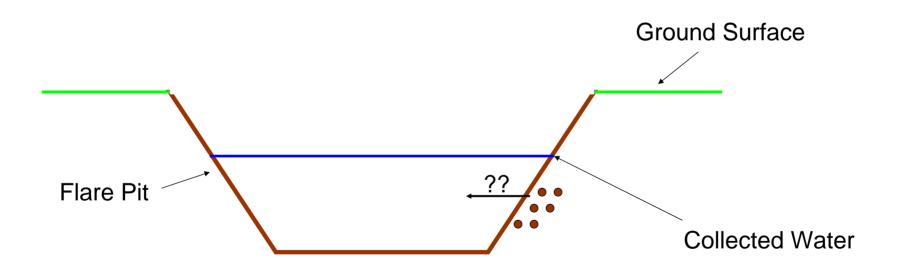
Is there a better way to handle this type of water?

In 2000, began sampling the collected water and found that despite soil impact, water was relatively clean





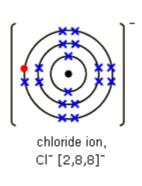
Is there a way to predict the amount of contaminants that would transfer from the soil to the collected water?

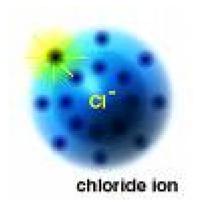


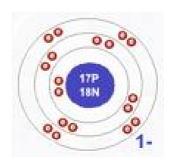




- Used a combination of three methods:
 - Case study data
 - Numerical model
 - Fick's Law Calculations
- Used chloride due to its conservative nature













- Case Study Sites
 - 17 sites were used
 - information regarding flare pit surface area, volume of collected water in excavation and soil and water chemistry







Case Study Sites

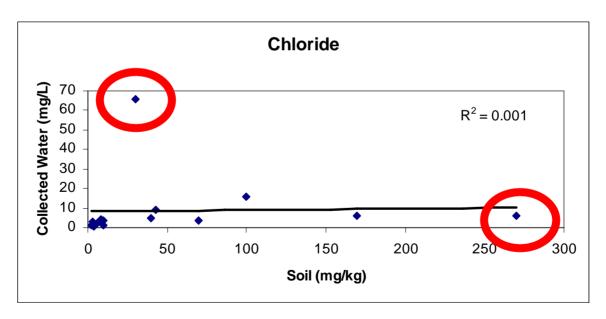
- Average chloride concentration found in soil was 51.5 mg/kg
- Average chloride concentration found in collected water was
 8.6 mg/L





Case Study Sites

 There was no correlation between concentrations of chloride found in the soil and the concentration found in the collected water



Numerical Model

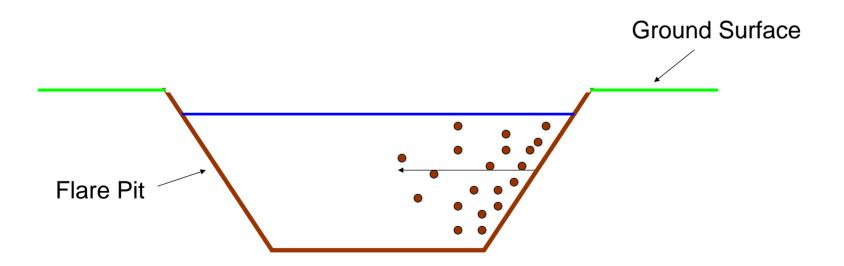
- Used ModFlow
- Used case study site data and published values to populate the model
- Started with 1000 mg/kg of chloride in the soil and ran the model for 1 year





Numerical Model

 After 1 year the predicted concentration of chloride in the simulated excavation was <10 mg/L







Calculations

- Used Fick's First and Second Laws to calculate flux ranges
- Concentration of a diffusing substance over an area and time





Results

$$F = -D_d \left(\frac{\partial \mathcal{C}}{\partial x} \right)$$

 $D^* = \omega D_d$

Where,

Where,

 $F = \text{mass flux of solute per unit area per unit time } (M/L^2T)$

 D^* = effective diffusion co-efficient (L²/T)

 $D_d = \text{diffusion coefficient } (L^2/T)$

 ω = coefficient related to porosity and tortuosity (unitless)

C =solute concentration (M/L³)

 $\left(\frac{\delta C}{\delta x}\right)$ = concentration gradient (M/L³/L)

$$\frac{\delta C}{\delta t} = D * \frac{\delta^2 C}{\delta x^2}$$

Where,

$$\frac{\delta C}{\delta t}$$
 = concentration over time (M/L²T)

 D^* = effective diffusion co-efficient (L²/T)

$$\frac{\delta^2 C}{\delta x^2} = \text{concentration gradient } (M/L^3/L)$$



Results

$$F = -D_d \left(\frac{\delta C}{\delta x} \right)$$

Where,

 $F = \text{mass flux of solute per unit area per unit time } (M/L^2T)$

$$D_d = \text{diffusion coefficient } (L^2/T)$$

C =solute concentration (M/L³)

$$\left(\frac{\delta C}{\delta x}\right)$$
 = concentration gradient (M/L³/L)

$$D^* = \omega D_d$$

Where,

 D^* = effective diffusion co-efficient (L²/T)

 ω = coefficient related to porosity and tortuosity (unitless)





$$\frac{\delta C}{\delta t} = D * \frac{\delta^2 C}{\delta x^2}$$

Where,

$$\frac{\delta C}{\delta t}$$
 = concentration over time (M/L²T)

 D^* = effective diffusion co-efficient (L²/T)

$$\frac{\delta^2 C}{\delta x^2} = \text{concentration gradient (M/L}^3/\text{L})$$





Using three methods all results were below:

500 mg/L (Health Canada, 2006)

230 mg/L (AENV, 2009 - Natural Area)

100 mg/L (AENV, 2009 – Agriculture, Irrigation)







- An application was made to the ERCB for the "surface discharge of collected water to adjacent lands".
- A rigorous sampling protocol and analytical schedule for collected water was developed and approved by the ERCB.
 - water can not have a visible sheen
 - each sample analyzed for hydrocarbons, routine potability and contaminants identified in the excavation
 - landowner acceptance of analytical data and discharge area





- ► The application of the protocol is cumbersome
 - precipitation events are unpredictable
 - lab turn around time on samples
 - landowner availability for approval prior to discharge







Best available practice for the time being







In the future, collected water should fall under a generic guideline and a discharge protocol set up similar to retention ponds at oil and gas facilities.





This would ensure that the water is not removed from the hydrological cycle and the most is being made of this scarce resource.





Thank You



▶ Dr. L. Bentley, University of Calgary



M. Morden, Petro-Canada



▶ M. Bowles, Golder and Associates Ltd.





WorleyParsons

resources & energy